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Practical Characterisation of the Piezo Electric Properties of a 3K T300 Carbon Fibre for Impact Sensoring

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Abstract—This paper discusses the results obtained during the practical characterization of the piezo electric properties of a commonly used carbon fibre. The aim of the investigation was to prepare the grounds for the feasibility of a low cost impact sensor that could be included in any carbon fibre structure (megalthic or thin structure) without interfering the integrity of the actual structure itself. The entire measurement loop as well as the techniques of connectivity of the fibres to the loop is described within. The piezo electric effects and all factors which affect the measurements are reflected in the analysis. The results obtained shown that in normal laboratory conditions the piezo-electric response of a T300 carbon fibre is consistent and directly proportional to the impact applied to the fibre.

Keywords—*piezo electric effects; carbon fibre structures; low cost impact sensing*

I. INTRODUCTION

Nowadays, Carbon Fibre Reinforced Plastics (CFRP) are widely used in various industrial applications. Their advantages over many traditional materials have been demonstrated on many occasions. The manufacturing process of the CFRP has also been extensively investigated, including the cure of the composite using microwave heating [1]. The cure of the composite, particularly the thick elements, is proven to be a challenge during the production. A simple analogy to culinary science will be the cooking of cakes. The outside of any product are rarely warming up at the same pace as the inside: the outside cooks faster than the inside, resulting in a difference of baking pace, leading to structural differences and ultimately cracks on the outer surfaces of the baked cake [2].

The use of the traditional and Microwaves Techniques (MWT) of heating developed by Papaygaris et al. [1] allows uniforming temperatures across the section and a reduction of the internal stresses. Unfortunately, such MWT methods are incompatible with the use of the traditional temperature sensors. Any other sensing techniques, for stress monitoring (foil strain gauge) in particular, are also being made obsolete because of their reaction under MWT. They may also have a negative structural influence by generating point of stress concentration [3].

Furthermore, the Non Destructive Techniques (NDT) recently developed for measurement of defaults in CFRP are expensive and demanding for field applications.

With this in mind, the need for the development of a low cost, homogenous, stress sensor capable of measuring temperature changes and fast changes of stress (impact) is genuine. In order to do so, extensive study of the electrical characteristics of the commercially used fibres is needed [4].

II. METHODOLOGY

The methodology used for the evaluation of the electrical response of the fibre has been developed over numerous attempts of characterisation. As it stands, the testbed is made of a fixed aluminium beam on to which numerous elements are attached.

The choice of having a 1 m long test fibre came as natural. Some evaluations of the response of shorter specimens have been made; the response is proportional to the length of the sensing element since the stress/energy is equally distributed along the sensor. Having a 1 m long sensor made the quantification of the results easier and allowed to provide the data as “per meter” of sensor length [5].

Many techniques have been tested and benchmarked using modern accelerometers [6]. At first, the repeatability of the mechanical impact has been considered.

Stepper motors were initially preferred to create and control the movement of a fixed mass impactor, this was the best option to modify easily and conveniently the impacting energy. This option had to be aborted due to the negative effect on the stability and veracity of the measurements linked to the Electromagnetic Interferences (EMI) that the motors were generating [7]. The pneumatic option for the actuation of the impactor has been selected because of its relative convenience of use (variation of the speed), it offers a good repeatability (measured systematic error under 0.5%, random under 1%).

The measurement loop is very traditional and consists of a Vishay scanner for strains/micro-voltages. The connections between the sensing fibres and the measurements loop have also been evaluated. Many options had to be assessed including

gold plating of the connection area. Existing silver based epoxies have shown extremely good advantages over gold plating, in particular for field use.

Silver based epoxies are however incompatible with the MWT due to their structures. An innovative compound compatible with all existing curing methods and NDT has been developed using carbon nanotubes (Patent under review).

Fig. 1 below shows the latest test bed capable of creating longitudinal impacts on a fibre.

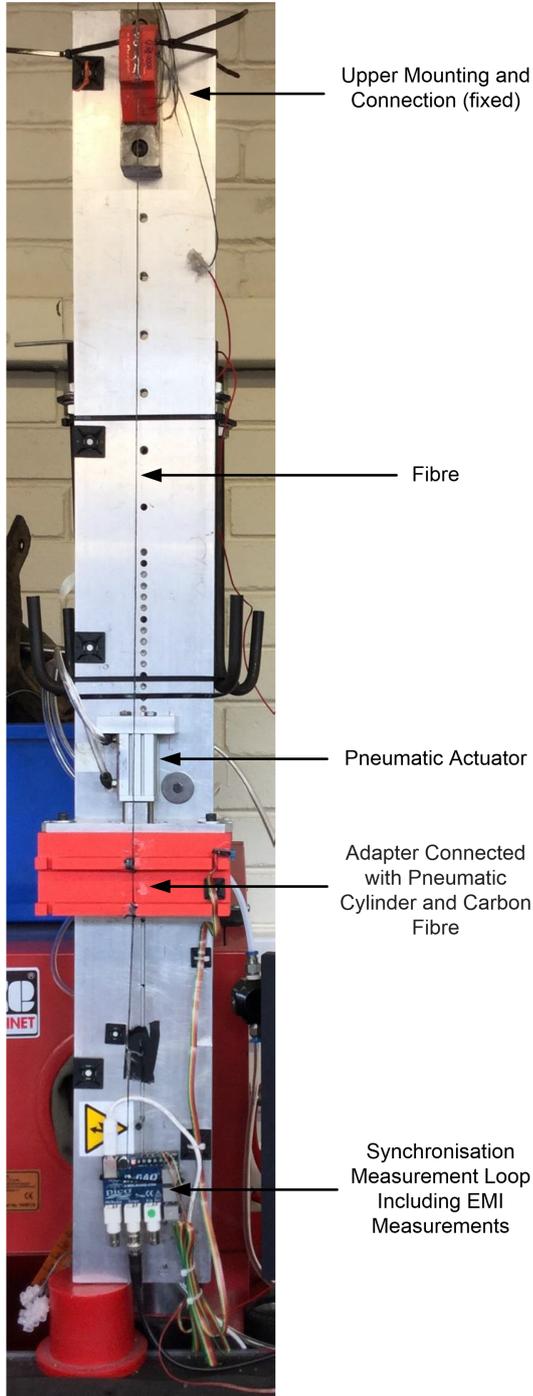


Fig. 1. Test bed

III. MEASUREMENT TECHNIQUES

Fig. 2 and 3 shows the results of the preliminary tests done in order to validate and calibrate the measurement technique. ΔT_1 is the delay time occurring after the initiation of the impact and the beginning of the response of the carbon fibre. ΔT_2 is the time which to reach the maximum amplitude. T is the reaction occurring after initiation to the maximum amplitude of the measurement. V is the measured value for the difference of electrical potential between the upper and lower mounting areas. ΔV is the voltage change of the piezoelectrical effect occurring at two points in time.

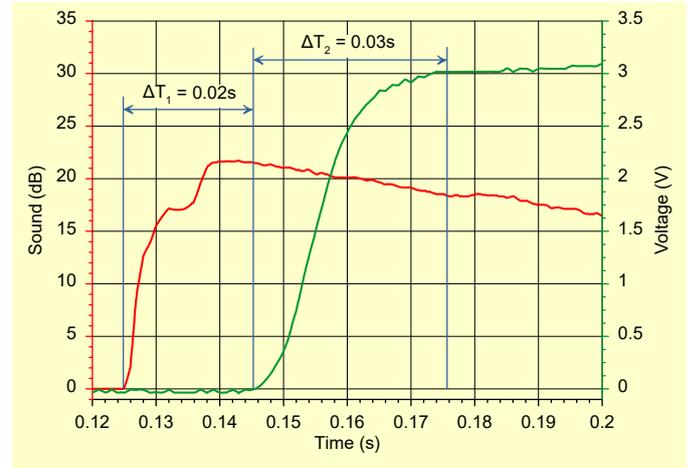


Fig. 2. Standard charge behaviour.

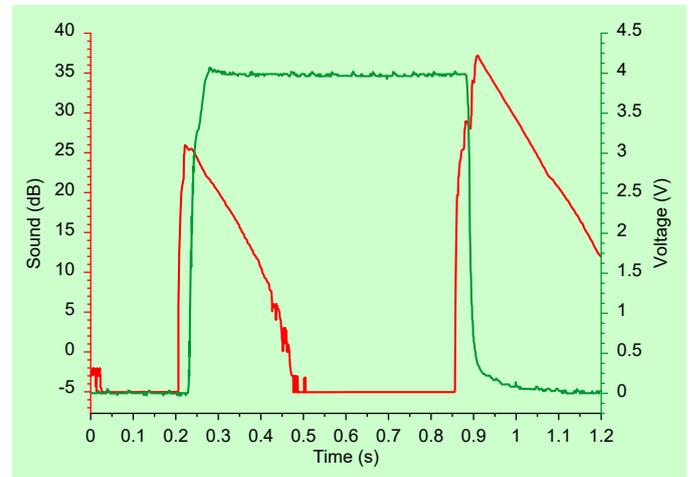


Fig. 3. Response of a 3K T300 fibre to fast application and release of longitudinal impact of 10 J.

Fig. 3 shows a 3K T300 fibre subjected to 10 J of impact. Two movements are shown, in red is the actuation in the form of a spine. The first movement (at time 0.2 s) is a tensional load while the second (at 0.85 s) is the release of the stress. The green line depicts the potential change of the carbon fibre and shows an amplitude of approximately 4V.

IV. OBSERVATION

Fig. 3 shows interesting phenomenon. The sudden increase of response resulting in an overshoot (zoomed in Fig. 4) of the expected difference of potential is the characteristic of the

piezo-electric response of the material in this specific load scenario.

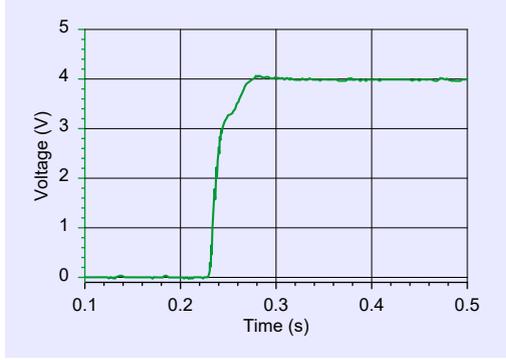


Fig. 4. Detail of Fig 3 showing the observed overshooting of the potential difference

The effect was amplified by the data acquisition loop. The amplification and attached filtration allow the removal of the unwanted EMI. [7] The power gain calculated using voltage instead of power using the Joule's law is:

$$Gain(dB) = 10 \log \frac{V_{out}^2 R_{in}}{V_{in}^2 R_{out}} \quad (1)$$

The gain used for the measurement was equivalent to a 10^3 factor. The filtration of the EMC was realised using a combination of low-pass and high pass filtration.

The Table I below shows the actual measurements obtained from a series of 7 tests. No measurements over $\pm 5\%$ from the median value have been measured in normal conditions.

TABLE I. MEAN COLLECTED DATA AND WORKED OUT VALUES FOR 10 J

Time (ms)	Loop Output (V)	Differential (V)	Unamplified value (V)
15	1.354		
31	4.067	0.094	0.094
47	4.123	0.15	0.15
62	4.098	0.125	0.125
78	4.058	0.085	0.085
93	4.032	0.059	0.059
109	3.994	0.021	0.021
125	3.976	0.003	0.003

At $T = 0$, the loop output (pure output of the measurement loop) is 0V. The impact time is 109 ms in duration on average. This is the measured time for the release of the 10 J through the fibre. The differential voltage announced in Table I is calculated using the following equation:

$$Diff.Out(T) = LoopOut(T) - LoopOut(after T = 0.125s) \quad (2)$$

The unamplified output is calculated by inverting the power gain equation announced above. The application of Ohm's laws for conductor gives:

$$P = \frac{V^2}{R} \quad (3)$$

where P is the power measured, V is the voltage measured and R is the resistance of the measured conductor (here 120 Ω).

The equivalent Energy developed by the piezo conductor can be evaluated using the Power (evaluated from the differential output at anytime over the duration of the impact) [8]. Since the differential output is varying over the duration of the impact, the simplest way of determination of the power over the impact is therefore:

$$E_{piezo} = \int_{t=0}^{\text{end of impact}} P dt = \int_{t=0}^{\text{end of impact}} \frac{V^2}{R} dt \quad (4)$$

In reality, the summation of the various (V^2/R) can be simplified in:

$$E_{piezo} = \sum \frac{V^2}{R} (t_{n+1} - t_n) \quad (5)$$

where t_n are the time at which every measurement was made.

The value obtained for E_{piezo} for an impact of 10 J is 6.41 W·s. The value of the impact was 10 J (10 W·s), is it therefore acceptable to announce that around 65% of the mechanical energy that the sensor has been subjected to has been transformed into electrical energy and measured as such.

Similar experimentations have been conducted for 5 and 20 J impact. Tables II and III show the results obtained for those impacts respectively. Using the same analytical analysis, the value obtained for E_{piezo} for an impact of 5 J is 3.16 W·s.

TABLE II. MEAN COLLECTED DATA AND WORKED OUT VALUES FOR 5 J

Time (ms)	Loop output (V)	Differential (V)	Unamplified value (V)
15	0.689		
31	2.098	0.032	0.032
47	2.151	0.085	0.085
62	2.134	0.068	0.068
78	2.122	0.056	0.056
93	2.092	0.026	0.026
109	2.078	0.012	0.012
125	2.067	0.001	0.001

TABLE III. MEAN COLLECTED DATA AND WORKED OUT VALUES FOR 20 J

Time (ms)	Loop output (V)	Differential (V)	Unamplified value (V)
15	2.71		
31	8.14	0.183	0.183
47	8.255	0.293	0.293
62	8.21	0.247	0.247
78	8.121	0.157	0.157
93	8.068	0.105	0.105
109	7.994	0.031	0.031
125	7.964	0.002	0.002

E_{piezo} calculated from the above data, for an impact of 20 J, is 13.83 W·s. Table IV shows the different values of harvested energy for various longitudinal impacts as well as the response of the system in W·s/J (calculated using the mean values of the measurements).

TABLE IV. REVIEW OF THE RESPONSE

Impact Developed (J)	5	10	20
Energy harvested (W·s)	3.16	6.41	13.83
Response (W·s/J)	63.2%	64.1%	69.2%

Between 5 and 20 J, a relative consistency in the ratio Energy measured/impact is noted. The current settings are refraining the production of accurate impacts over 25 J so it is, in the current state of play, impossible to conclude any further in the linearity of the response of the fibre to impact. It is, however, possible to note that the response of the fibre is, as predicted, linear between 0 and 20 J.

V. CONCLUSIONS

This investigation observes that, in normal laboratory conditions (at a constant temperature of 20°C and a normal degree of hygrometry) the piezo-electric response of a T300 carbon fibre is consistent and directly proportional to the impact applied to the fibre. The measurement of the piezo-electric response was realised using traditional strain equipment and evaluated by focusing on the overshoot of the response of the conductor. The stain gauge effects of the carbon fibres (in particular the gauge factor) have voluntarily

been neglected from this analysis, as they do not offer any novelty in their study, the overshoot in the response is the only point of focus in the evaluation of the piezo-electric effect. The investigation has shown that the amount of overshoot (area of the measured response – stabilised response) is proportional to the speed at which the stress is applied (impact). It is therefore possible to conclude that the fibre can be used as a strain as well as an impact sensor for further development.

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